



GLWA WRF 5069 Kercheval Cast Iron Pipe Pilot:

Steel Composite Liner, of 108-year-old 48" cast iron water main with embedded real time structural health

monitoring



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Great Lakes Water Authority (GLWA) was formed out of the 2013 bankruptcy of Detroit

- •The "Grand Bargain" for Detroit Renaissance and Emergence from the Ashes of Bankruptcy
- Began operation on January 1, 2016
- Regional wholesale provider for water and wastewater with 120+ member partners
- •GLWA has been recognized as an innovative and world class water system

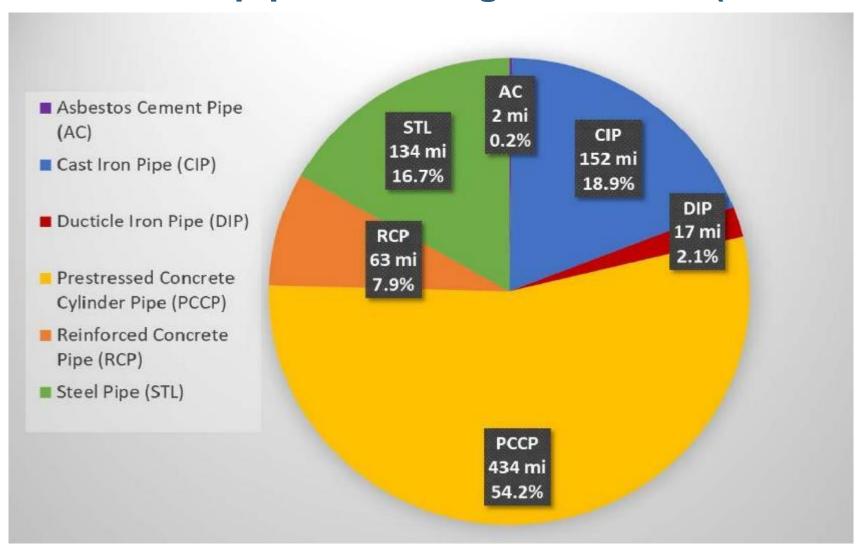








GLWA is the Largest Domestic Owner of PCCP and allof their pipes are Large Diameter (>24 inch)



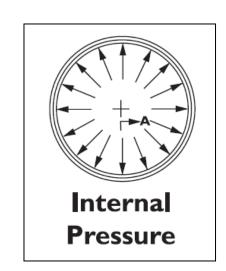
For ANY TYPE OF PIPE, Renewal Process Begins by with how much renewal is needed

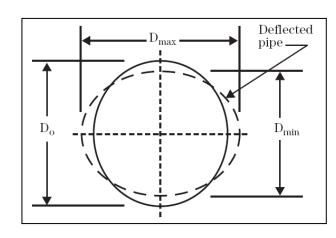
Renewal

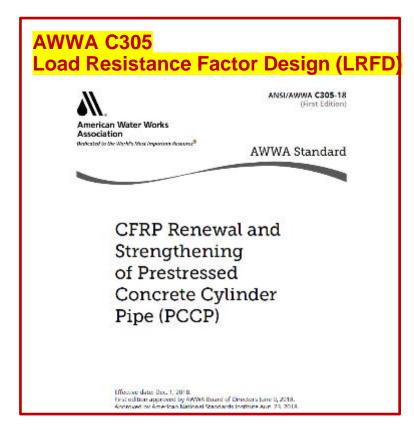
	Rehabilitation			Kenewai
Liner Characteristic	Structurally Interactive			Structurally StandAlone
	Internal Coating	Hole and gap span	Hole and gap span + ring stiffness	Structural Resistance for all specified loads (Does Not Rely on Host Pipe)
AWWA Classification	Class I	Class II	Class III	Class IV
Internal corrosion protection	V	V	✓	✓
Reliable adhesion to host pipe	V	V		
Hole and gap span at maximum allowable pressure (MAOP)		•	•	✓
Inherent ring stiffness (hydrostatic pressure loads)			~	✓
Positive connection to service taps and sealed at other discontinuities (water tightness)			*	
Inherent ring stiffness (all external and vacuum loads)				✓
Pressure rating of liner ≥ MAOP of host pipe				✓
Liner survives host pipe failure				V

Design Methodologies should be consistent between renewal methods

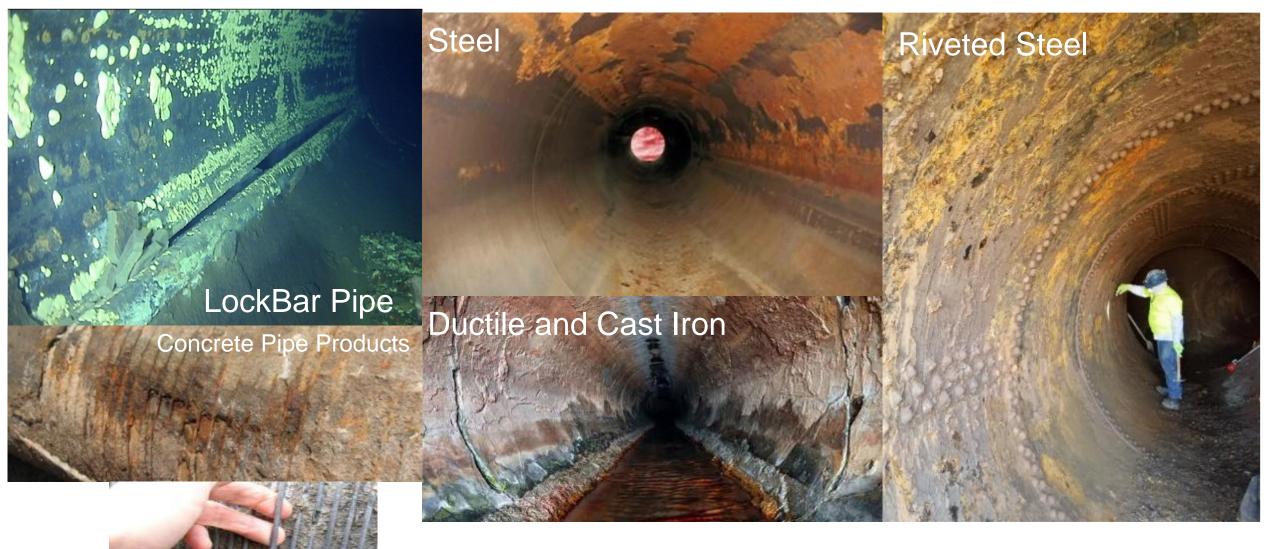
- ✓ Internal working pressure
- ✓ Internal working-plus-transient pressure
- ✓ Weight of pipe and fluid
- ✓ Earth load above the pipe
- ✓ Live loads at the ground surface
- ✓ Groundwater above the pipe
- ✓ Negative pressure inside the pipe
- ✓ Poisson's ratio
- √ Temperature changes
- √ 50 + year Design Life







AWWA Class IV Systems need to be designed to cover a broad range of specific pipe types and their failure mechanisms



All Design Methodologies are NOT equivalent

ASTM F1216 - Appendix X1 Allowable Stress Design (ASD)



Designation: F1216 - 09

An American National Standard

Standard Practice for Rehabilitation of Existing Pipelines and Conduits by the Inversion and Curing of a Resin-Impregnated Tube^{1, 2}

APPENDIXES

(Nonmandatory Information)

X1. DESIGN CONSIDERATIONS

X1.1 Terminology:

X1.1.1 partially deteriorated pipe—the original pipe can support the soil and surcharge loads throughout the design life of the rehabilitated pipe. The soil adjacent to the existing pipe must provide adequate side support. The pipe may have longitudinal cracks and up to 10.0% distortion of the diameter. If the distortion of the diameter is greater than 10.0%, alternative design methods are required (see Note 1).

X1.1.2 fully deteriorated pipe—the original pipe is not structurally sound and cannot support soil and live loads or is expected to reach this condition over the design life of the rehabilitated pipe. This condition is evident when sections of the original pipe are missing, the pipe has lost its original shape, or the pipe has corroded due to the effects of the fluid, atmosphere, soil, or applied loads.

$$P = \frac{2KE_L}{(1 - v^2)} \cdot \frac{1}{(DR - I)^3} \cdot \frac{C}{N}$$
(X1.1)

where:

P = groundwater load, psi (MPa), measured from the invert of the pipe

K = enhancement factor of the soil and existing pipe adjacent to the new pipe (a minimum value of 7.0 is recommended where there is full support of the existing pipe)

E_L = long-term (time corrected) modulus of elasticity for CIPP, psi (MPa) (see Note X1.1),

ν = Poisson's ratio (0.3 average),

DR = dimension ratio of CIPP,
C = ovality reduction factor =

AWWA C305

Load Resistance Factor Design (LRFD)



CFRP Renewal and Strengthening of Prestressed Concrete Cylinder Pipe (PCCP)

Effective date: Dec. 1, 2018.

First edition approved by AWWA Board of Directors June 9, 2018.

Approved by American National Standards Institute Aug. 23, 2018.

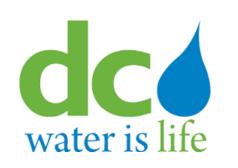
LRFD approach embodied in AWWA C305 (CFRP) for PCCP Renewal has been adopted and implemented by many water utilities

- Major US water agencies have adopted the use of the CFRP technology as part of an effective asset management program
- LRFD design methodology is also adopted in many other design standards and MOP for ASCE for Penstocks and large diameter gravity pipe renewal.
- AWWA C305 has significantly reduced risk associated with large diameter pipe renewal



Santa Clara Valley Water District



















ASTM F1216 (ASD) is not equivalent to AWWA C305 (LRFD) for Large Diameter Pressure Pipe

Design Checks	ASTM F1216 (ASD)	AWWA C305 (LRFD)
Hoop Design		
Internal Working Pressure	X	X
Internal Transient Pressure		X
Internal Vacuum Pressure		X
External Soil Load	X	X
External Traffic Load	X	X
Pipe Ovality	X	X
Deflection Limit		X
Combined Loading		X
Longitudinal Design		
Poisson's Ratio Effect		X
Temperature Change Effect		X
Thrust Effect		X
Design Life up to 50 Year?		X

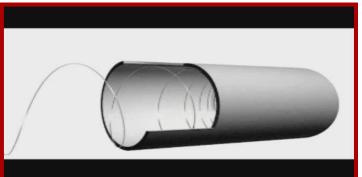
GLWA objectives of pilot are focused on liner application and monitoring methods

TICKLE COLLEGE OF ENGINEERING

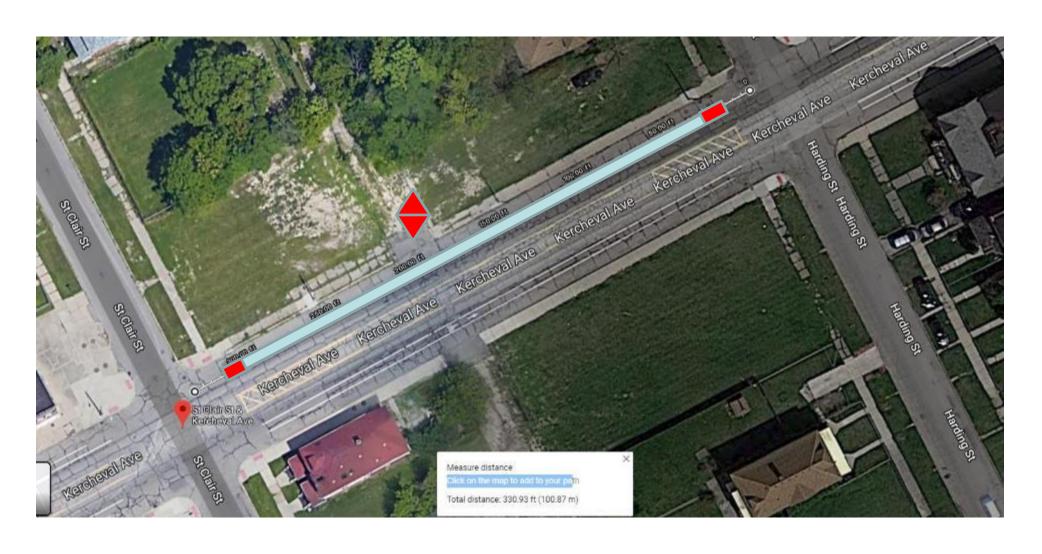
- Applied research on innovative, emerging technologies for Class IV renewal of large diameter pipe
 - Polymer-based System (MICP)
 - Steel Reinforced Cement Mortar (StrongPIPE SRC)
- Collect experience and information on
 - Design Methodology for Class IV Liner Systems
 - Production means and methods
 - Costs and Lessons Learned
- Conduct structural monitoring of systems
 - Laboratory of Intelligent Systems Technology
 - Dr. Jerry Lynch







GLWA Located an accessible portion of their Kercheval Avenue, 1913 Vintage, 48 inch diameter Cast Iron Pipe (CIP) for the renewal pilot

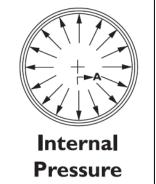


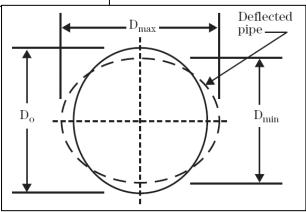
All Candidate Liner Systems were designed using LRFD

methodology

- Class IV, structurally independent renewal
- 48-inch, 1912 vintage Cast Iron Pipe (Class D)
- "flat, straight pipe", (per GLWA 1912/1913 field notes)
- Open cut excavation access on one or both ends of segment
- Working Pressure (max): 100 psi (actual operating 70 psi)
- Surge Pressure: +40 psi
- Depth of Cover to Crown: 10 feet
- Groundwater: No
- Water temperature change: Δ25 C = Δ40 F
- Internal surface condition like that of 42-inch samples provided by GLWA









Results of LRFD "Apples to Apples" Comparison Lir Thicknesses were interesting and informative in decision making process

- LRFD designs resulted in liner thicknesses:
 - CFRP 3 circumferential wraps and 1 longitudinal layer (0.6 " thick)
 - SCL with thickened epoxy embedment (0.75" thick)

60 LF

SCL with cementitious embedment (~1" thick)

132 LF

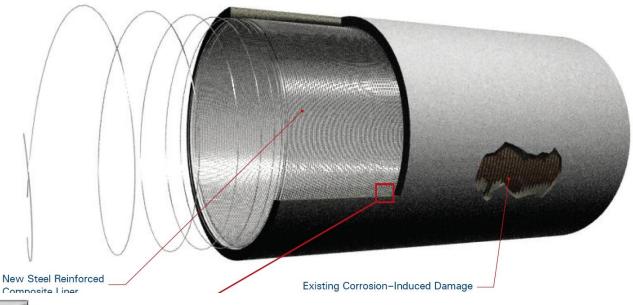


HDPE (2.3" thick)

to provide stand alone, full-structural reinforcement per the requirements of AWWA Manual M28 Class IV.

StrongPIPE® SCL Solution utilizes cost effective HS steel for trenchless composite reinforcement since 2012





StrongPIPE System

Existing Pipe

2

Legend

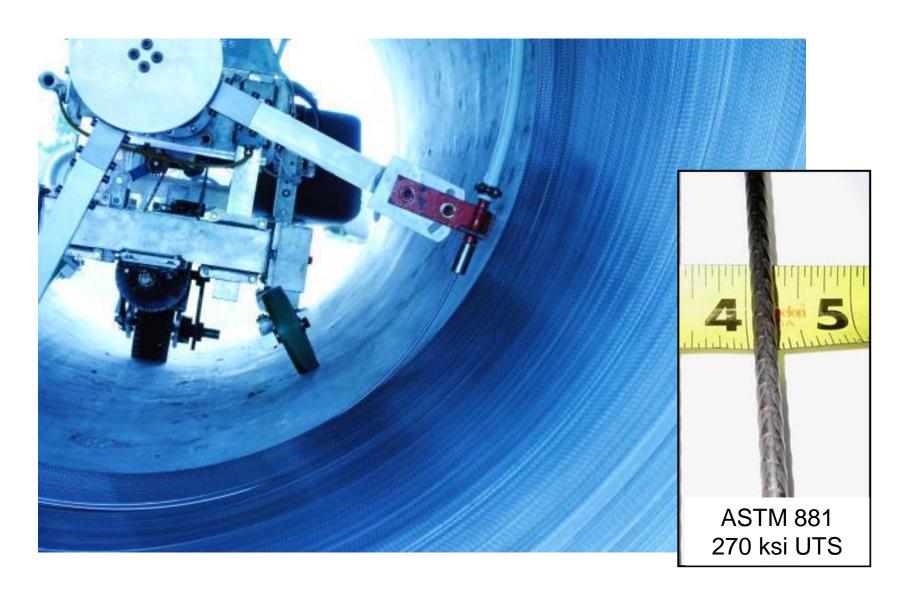
- 1st Glass FRP Layer (longitudinal)
- 2. High Str. Steel Wire
- 3. Polymer Matrix
- 2nd Glass FRP Layer (longitudinal)
- 5. Flexible Topcoat

StrongPIPE is a structural strengthening system for the **restoration** of damaged/weakened pressure pipe and the **upgrade** of undamaged pipe. **StrongPIPE** utilizes a continuously wound tensile reinforcement that forms a steel composite lining inside the existing pipe.

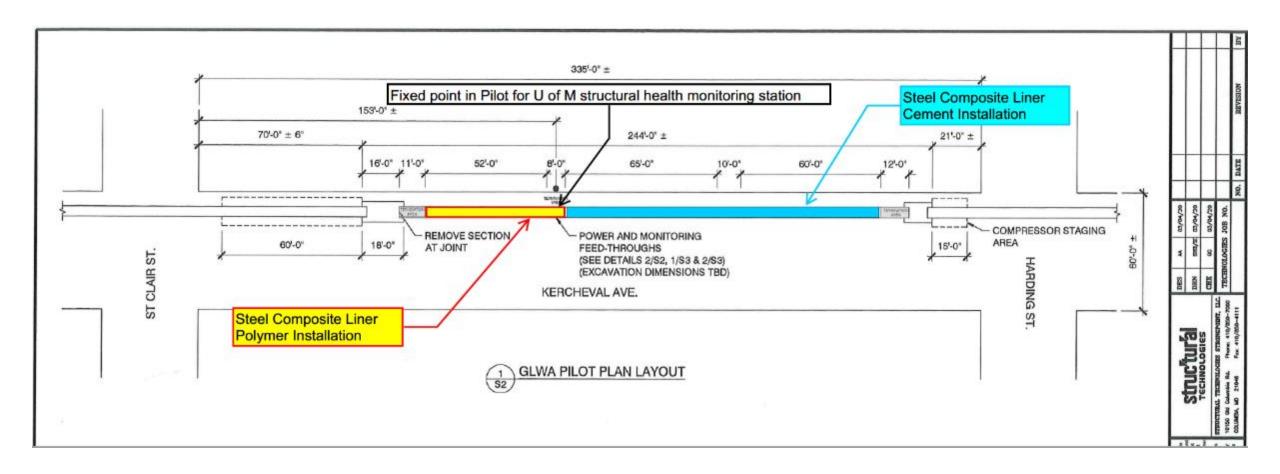


Steel Composite Liner Systems use high strength wire embedded in a host matrix to provide primary circumferential strength renewal

- Longitudinal strength from HS steel, FRP or CFRP.
- Applicable for large diameter pressurized and non-pressurized pipelines (36 inches in diameter and up).
- Applicable for either targeted repairs or extended, straight runs.
- Installed through existing access.
- Similar structural strength to CFRP, but more cost effective for longer runs
- NOT PCCP

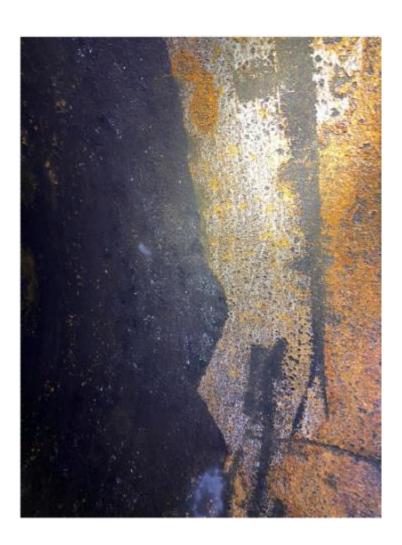


Final layout was SCL with 1/3 polymer and 2/3 cementife embedment



Internal surfaces were prepared by scraping, high pressure water blasting and abrasive blasting to receive lining systems

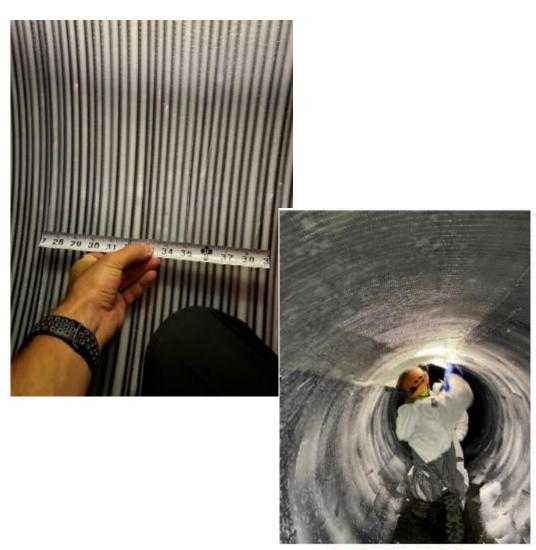






Circumferential wire spacing was the same for SCL-C and SCL-P



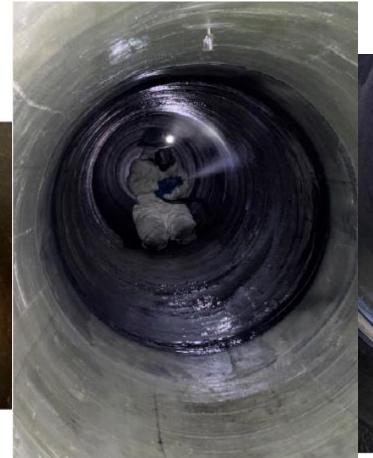






Spin cast mortar over SCL-C wires and top coat with polyurea and end seals for water tightness

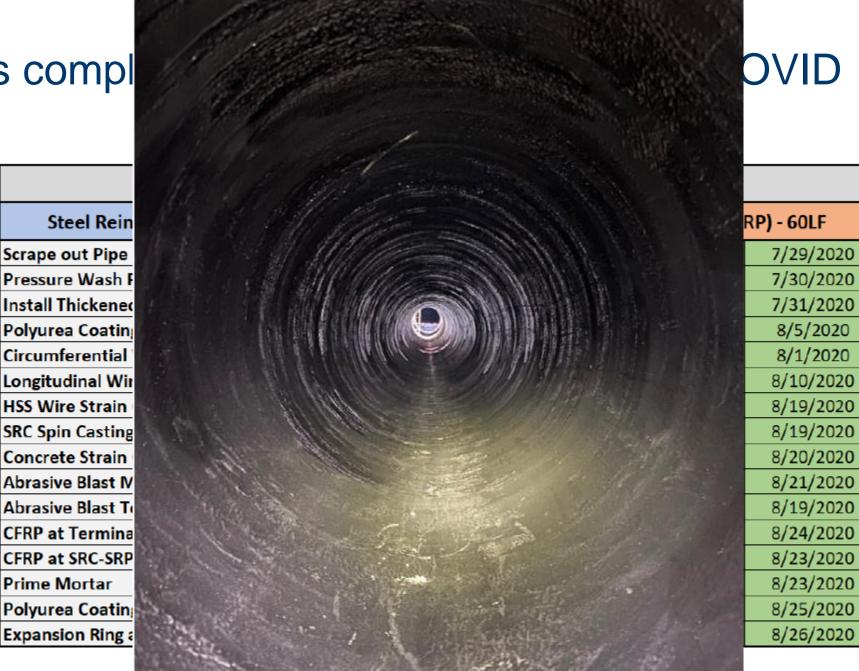






Pilot was compl

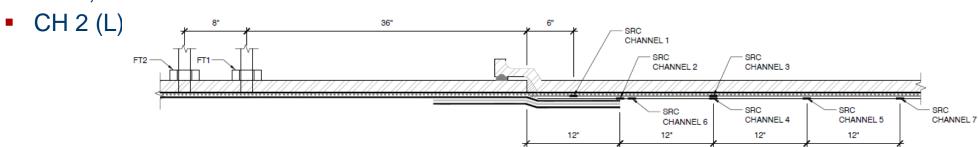
Prime Mortar

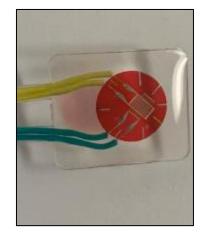




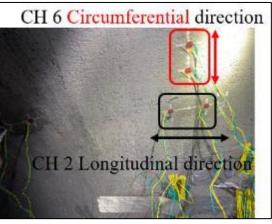
GLWA/UofM Kercheval Pilot is a first of its kind in situ pipe health monitoring system

- Seven (7) strain channels on the SCL-C liner:
 - CH 1, CH 3. CH 5. CH 7 on steel wires (auarter bridge)





Rosette gages in polymer substrate



Full-bridge (thermally compensated) gages for circumferential and longitudinal strain

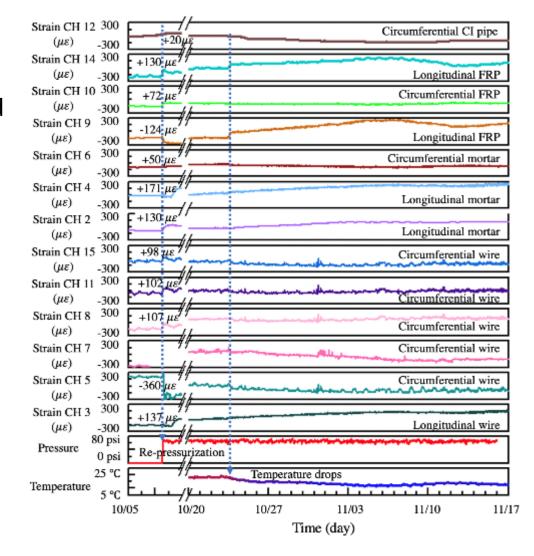


Polyimide substrate gage (quarter bridge) on wire

System Data Collection

Data collected since August 26, 2020:

- All strain channels zeroed
- Data collected at 2 kHz
- Collect data for 1 second every 5 minutes
- Locally stored on DAQ server at the site
- Transmitted by cable modem to UM server ever day
- Backup copy of the data stored in external hard drive at the site



Observable Behaviors

Internal pressure response:

- Negative longitudinal strain
- Positive circumferential strain

Constraints at the pipe-liner end:

Longitudinal strain

Thermal contraction:

- Negative circumferential strain
- Positive longitudinal strain

Liner cracking (mortar):

- Cracks along circumferential direction increases ε_{χ}
- Cracks along longitudinal direction increases ε_{θ}

Deformations over time:

- Long-term creep
- Less support from soil
- Both strains increase as time goes by

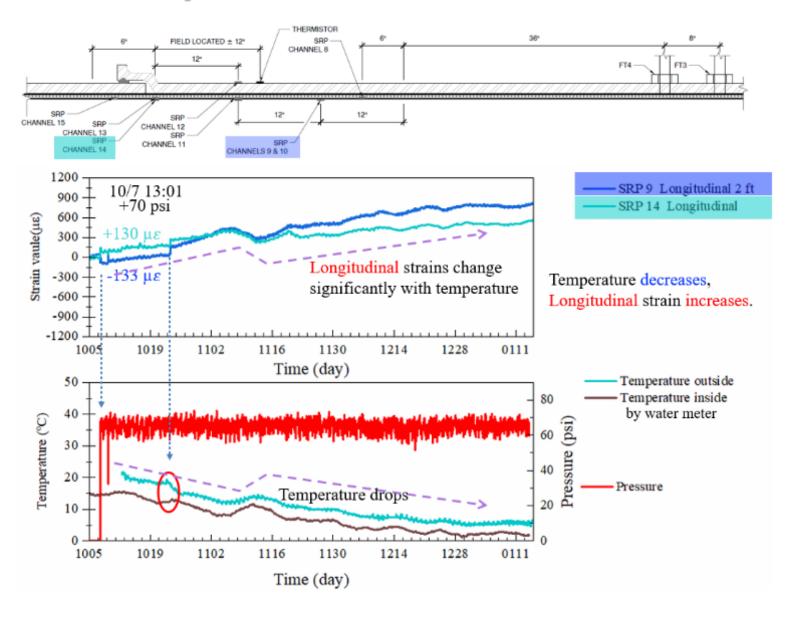
Related to pressure, and boundary conditions

Temperature-driven behavior (seasonal)

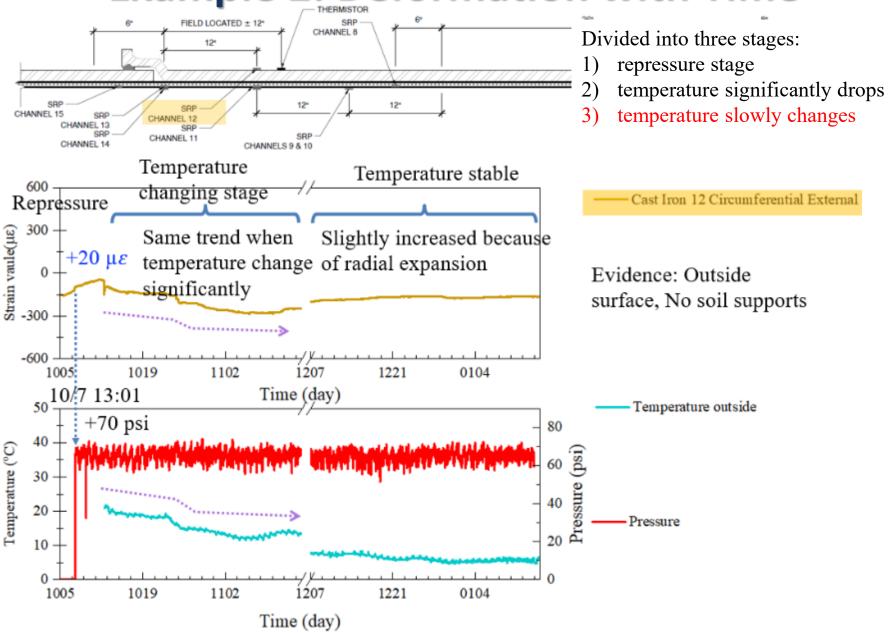
Transient event driven

Long-term, slow deformation

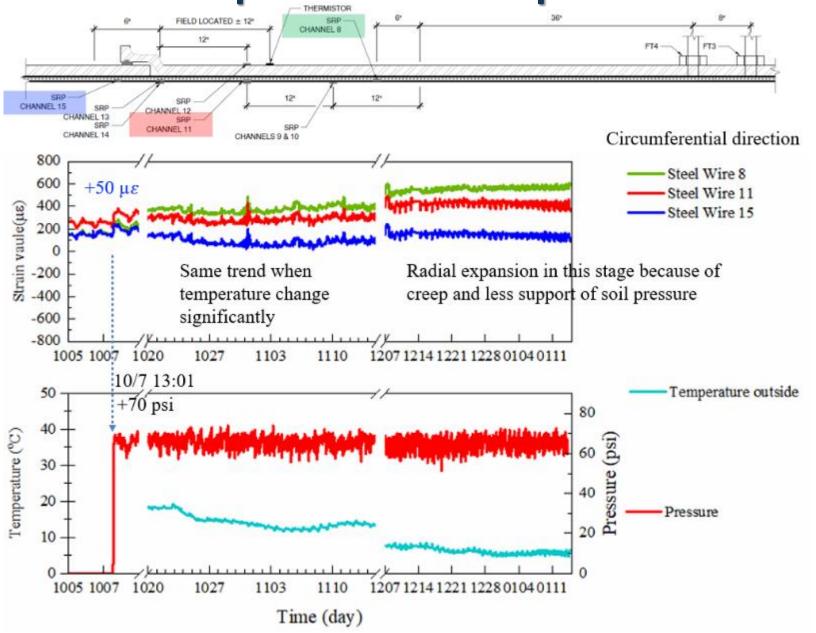
Example 1: Thermal Contraction



Example 2: Deformation with Time



Example 3: Radial Expansion



Many thanks to my colleagues John Norton, Todd King, Ali Alavi, Wentao Wang, and Jerry Lynch

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